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STANDARDFOR WELDING, BRAZING, ANDFUSING OPERATORSASME Boiler and Pressure Vessel Committee Brazing, and FusingAN INTERNATIONAL CODE2017 ASME Boiler and Pressure Vessel Code2017 Edition July 1, 2017Two Park Avenue New York, NY 10016 USADate of Issuance: July 1, 2017 This international standard was developed under accredited procedures as meeting U.S. national standards and is a U.S. national standard. The Standards Committee that approved the code or standard was balanced to ensure that competent and relevant persons of interest had the opportunity to obtain additional input from industry, academia, regulators and the general public. ASME does not approve, evaluate or approve any element, construction, proprietary device or activity. ASME takes no position as to the validity of the patent rights claimed with respect to the anyitems mentioned in this document, nor to assume such liability. 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The American Society of Mechanical Engineers Catalogue Card Number: 56-3934Printed in the United States of American Society of Mechanical Engineers, 1914; Latest edition 2017. The American Society of Mechanical Engineers Catalogue Card Number: 56-3934Printed in the United States of American Society of Mechanical Engineers, 1914; Latest edition 2017. The American Society of Mechanical Engineers Catalogue Card Number: 56-3934Printed in the United States of American Society of Mechanical Engineers, 1914; Latest edition 2017. The American Society of Mechanical Engineers Catalogue Card Number: 56-3934Printed in the United States of American Society of Mechanical Engineers (Automatical Engineers) and the United States of American Society of Mechanical Engineers (Automatical Engineers) and the United States (Automatical Engineers) and Engineers Two Park Avenue, New York, NY 10016-5990 Copyright 2017 by The AMERICAN SOCIETY OF MECHANICAL ENGINEERS all rights reserved for the list of articles . . xForeword . xiiStatation of the policy on the use of the certification mark and code authorization in advertising . 14Throdation of the ASME Marking Policy to identify manufactured items. xivSubmittal technical investigations to the standards committees of boilers and vessels under pressure . 16th Person. xviiiIntroduction . xxxviiSummary of Changes in the Code of boilers and stylistic changes to the file number order . xlviiCross-Reference and stylistic changes in the Code of boilers and stylistic changes to the file number order . xlviiCross-Reference and stylistic changes in the Code of boilers and stylistic changes in the Code of boilers and stylistic changes in the Code of boilers and stylistic changes to the file number order . xlviiCross-Reference and stylistic changes in the Code of boilers and stylistic changes in the Code of boile 18QW-170 Toughness Tests . 19QW-180 FilletWeld Tests . 19QW-290 Character Bead Welding . 66Article II Welding Performance 920W-430 FNumbers . 1630W-440 Welded Metal Chemical Composition . 1740W-450 Species . 1750W-460 Graphics . 180iiiOW-470 Etessente processes and reagents . 224Article V Standard Welding Procedure Specifications (SWPSs) . 4 comentions 0 gostaram Estat-sticas Notas Seja a primeira pessoa a gostar disto 1. T there significant changes that ap-pear in ASMEBoiler and Pressure Vessel Code, Section IX, 2017 Edi-tion, are discussed here. All changes can be easily identified in the Change Sum at the front of Section IX, 2017 Edi-tion, are discussed here. All changes can be easily identified by 17 in the margins; while most changes are easy to discern when reading a paragraph, in this edition there are more than 100 cases where affected heat arc. In addition, because there are hardness measurement methods other than charpy test-ing (e.g., drop weight and crack tip opening displacement (CTOD), the words impact test and notch hardness have been generally changed to simply robustness test. Part HQ, General Requirements have different requirements than those in Section IX; HQ-100 indicates documents that refer to Article IXtake pre-dence on Article IXrequirements. The last two paragraphs of HQ-101 were deleted because they had this upside down. They incorrectly stated that Section IX can be used with other sections of the Boiler Code and ASME B31, Pressurized Piping Code, and merely suggested that all the rules of these standards of re-garding welding qualification be taken into account. For those involved in the si-multaneous qualification of welders, HQ-106.3 has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition for leak gas has been revised editorially to make it easier to read; no significant changes have been made. An definition of welders, and the properties of the pr some mid- or editorial changes to some of the QW-408variables. In the last sentence of HQ-105.5, the 2015 edition stated the requalification 42 WELDINGJOURNAL / AUGUST 2017 What's Newin the ASME Boiler and Pressure Vessel Code Section IX This summary details the changes made to the 2017 edition of Awelder using the Putinaroot pass. BY WALTERJ. SPERKO 2. was necessary if a modification was made to the variables of the special welding processes of the overlay resistant to corrosion. This incorrectly stated that essential and non-essential variables require requalification, the last sentence of HQ-105.5 has been deleted. Welding Procedure (QW-200) Changes QW-200.4(b) provides some relief to QW-200.4(a) requirements to comply with the base metal thickness range and the thickness range are the thickness range and the thickness range are the thickness range and the thickness range are the thick, and a second PQR for a second qualified process on a test coupon at least 1/2 inch thick to support a WPS that allows both processes to be used to weld base metals from 16 to 8 inches thick. QW-200.4(b) is an exception to QW-451 re-quirements, the following sentence was moved from the middle of QW-200.4(a) at the beginning of QW-200.4(b): Alternatively, the qualification of WPS for root deposits only can be made in accordance with (b). There are occasions when corro-zionist welding metal overlay has been added to one part and the construction requires welding another part to this overlay following a different WPS. Since the overlay has no p-number assigned to it, a new paragraph has been added to the QW-211 al-lowing welding metal overlay. Although there are many editorial changes to the tables in QW-250, the nonessential variable QW-409.8 has been added to special process tables for overlay welding. This variable requires that the current type and polarity be dressed on the STP. Those who weld repair moulds and those who weld on other thickness of the quali-fied base metal to 1.1 times the thickness of the test coupon if the weld is treated with heat above the upper tem-perature (e.g., standardized) processing. QW-407.1 already requires that any thermal treatment the upper processing temperature is qualified, so there was no rational basis for limiting the thickness of the test coupon. A new welding process, low-power, low-density (LLBW) laser beam welding, has been added as QW-264.2, and details have been added in various other para-graphics, including a process definition and a new method of measuring heat input during its use. Although similar to ordinary laser beam welding (LBW), in LLBW the beam does not develop a keyhole and penetrates deep into the material. On the contrary, the beam is of low power and behaves more like gas tungsten arc welding than laser beam welding. The welds are made by adding heated filling metal to the resistance; the process will be used in the construction of the ship with a deep and very narrow groove, reducing the distortion as well as the amount of welding metal needed to do the job. For those who do temper the bead-ing weld, a fourth column C has been added to the temperamental bead variables in table QW-290.4 for use where the construction code specifies neither hardness test nor ha requirements for each pass, as required by QW-406.9, have been removed to test character bead coupons when impact tests were excessive. The QW-290.5(d) requirements were removed to test character bead coupons when impact tests were excessive. The QW-290.5(d) requirements were removed to test character bead coupons when impact tests were excessive. 403.6 is an additional es-sential variable that limits the mini-mom thickness of qualified base metal (i.e. 1/2 T). The test coupon had to be less than 1/4 inch (6 mm), the minimum qualified thickness of the test coupon or 5-8in., depending on the least. For thickness of the base metal (i.e. 1/2 T). The test coupon had to be less than 1/4 inch (6 mm), the minimum qualified thickness of the test coupon or 5-8in., depending on the least. For thickness of the base metal (i.e. 1/2 T). it-before, organizations would resort to purchasing 1/4-in.- (6-mm-) thick material and machining or grinding 0.010 inches (0.25 mm) or more on a surface to make the test coupon 0.24 inches (5.75 mm) thick. To address the need for this nonsense, QW-403.6 has been revised to say 1 inch (6 mm) or less. 4 When performing a voltage test we-ing a rectangular, the width of the test sample in the IXis section specified as about 3/4in. (16 mm); this is different from many other standards such as AWS D1.1 and ISO 15614-1, which specify that the width of the specimen is 1 inch (25 mm) wide in the rededuce section. If an organization wants to qualify to meet Section IXre quirements and also other Stan-dard requirements on a single test coupon, an additional set of voltage tests had to be prepared. In this edition, voltage test samples that meet the dimensional requirements of any of the following standards may be used; however, the stan-dard acceptance of Section IXstill applies: a)AWSD1.2 d) AWSD1.3 e AWSD1.6 f) FR-ISO4136 g) JIS Z3121 h) GB/T2651 i)NAVSEA S9074 AQGIB010/248. You will find that QW-402.30, QW-403.31, and QW-404.54 have been removed and you will have a hard time knowing which process was affected. Looking at the 2015 edition will not answer this question because they were removed in 2015 and replaced by generic rules in QW-220 that apply when using more than one welding process in the same welding bath. WeldingQualification (QW-300) Changes When radiography of a weld, QW-191 stated that demonstrating acceptable density and image quality on production or technical x-rays should be considered satisfactory proof of compliance with Article V, Article 2. The term density was removed from this paragraph, not because the cor-AUGUST2017/ WELDINGJOURNAL 43 3. rect density is no longer necessary, but because it was redundant — density is an integral part of section IXin 2010, there was concern that regular technicians would not be able to reliably identify defects if the test coupon was too thin. Under the direction V Committee, Section V Committee, Section V Committee, Section V committee decided to allow welders and welding operators to be qualified with test coupons up to 1/4 inch thick. Although the last two paragraphs of QW-191.2.2 imposing ASNTSNT-TC-1A and other personnel qualification requirements have been removed, these requirements have been removed, these requirements. The footnote 1 of Table QW-452 b) has been revised to align it with existing rules in qw-306. The previous note stated that the thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual thickness of the welding metal tension was based on the individual tension was always because the individual each welder or welding opera-tor, each welding process, and whenev-er there is a change in the welder, process and F-Number filling metal individually indeterminate of qualified thickness, but consider, if necessary, a change in progression, position, GMAW trans-iron mode and GTAWcurrent type when determining qualified thickness. There has been a significant effort to develop rules for welders qualified to make groove or net welds are also qualified to make sticky welds. In addition, a note was added to QW-461.9, the table that links the test position to the tread qualified welding positions: Peak welds are not limited by diameters of pipes or tubes when their aggreg length does not exceed 25% of the weld onto the hose in all positions he or she is qualified for. For connections, the design of the groove at the welder's qualifying diameter limits was clarified in QW-403.16: a) For a groove weld fixing a nozzle or branch, the qualified range of the QW-452.3 table must be based on the nozzle or branch, by For a groove weld fixing a nozzle or branch (with the preparation of the weld on the hull, head or operating hose), the qualified range of Table QW-452.3 must be based on the hull, the head or operating hose O.D. QW-322 on the continuity of qualifications for this process expire. Base metals and filling metals Some 26 new specifications and 82 new material categories were assigned p-numbers. A new metal filling specification has been added: SFA-5.36, Carbon and Low-Alloy Steel Electrodes for Flux Cored ArcWelding and Metal Cored Elec- trodes for Gas Metal ArcWelding. This standard will replace SFA 5.20 and 5.29 classifications, and contains an entirely new and more informative system for the allocation of AWS classifications. Nei-ther SFA-5.20 or SFA-5 existing wpss. Meanwhile, electrode manufacturers will identify their products with the two class sification systems in order to you can get used to the new classification system. Brazing Changes (QB) The only technical change in brazing was a revision of the QB-1 variable. Instead of postbraze thermal treatment (PBHT) QB-1. Instead of reading the same welding rules as he did for decades, only two conditions 1) Adding or removing a postbraze thermal treatment temperature over ± 25 degrees F (± 14 degrees Fahrenheit) or a change in post-brazing thermal treatment time of more than 15 minutes or 10% of the post-brazing thermal treatment time recorded on the PQR. Plastic Fusion (QF) Changes Paragraph QF-143 and Figure QF- 463 have been modified to correct the curvature angle for lateral curvature specimens. This angle has been changed from a maximum included angle of 60 ± 10 deg to 90 ± 10 deg to 90 ± 10 deg to be compatible with the ASTM F3183 specification, standard practice for guided lateral curvature assessment of polyethylene pipe buttFusion joints. Interpretations cfm. Possible ComingAttractions Low-energy discharge welding (LECD) is added to Sec-tion IX. Lecdwelding is used for at-tach thermocouple leads to piping to document preheating temperatures and post-ankle heat treatment. The rules re-quire that a WPS be prepared, but the qualification of the WPS is not re-quired, nor will the operators have to be qualified. There is an ongoing move to add more detailed visual examination re-stretches for welder test coupons. The current requirements are that incom-plete fusion, incomplete penetration, and cracks are not allowed. Section IXdoes has no additional requirements because organizations work according to different building codes, and the criteria for visual acceptance vary from code to code. This leaves the door open for organizations to impose acceptance criteria on their welders that are consistent with what welders will need to achieve when working on these other codes. The driving force behind this change is that some or-ganizations do not consider crite-ria, except what is in section IX, result-ing in welders who are qualified but not very qualified. This proposal is very resilient. Readers are informed that ASME Code Committee meetings are open to the public; The schedule is available on the author's website and asme.org. Errata and editorial corrections are displayed asme.org/kb/standards/ publications/bpvc-resources so that code users can easily see revisions and corrections. WJ WALTER J. SPERKO, P.E. (sperko@asme.org), is President, Sperko Engineering Services Inc. (sperkoengineering.com), Greensboro, N.C.He is also a general director of AWS. Readers are informed that the opinions expressed in this article are those of Sperko, and not the official opinion of ASME BPV Standards Committee IX. For more information, visit aws.org/adindex August 2017/ WELDINGJOURNAL 45 45 45

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